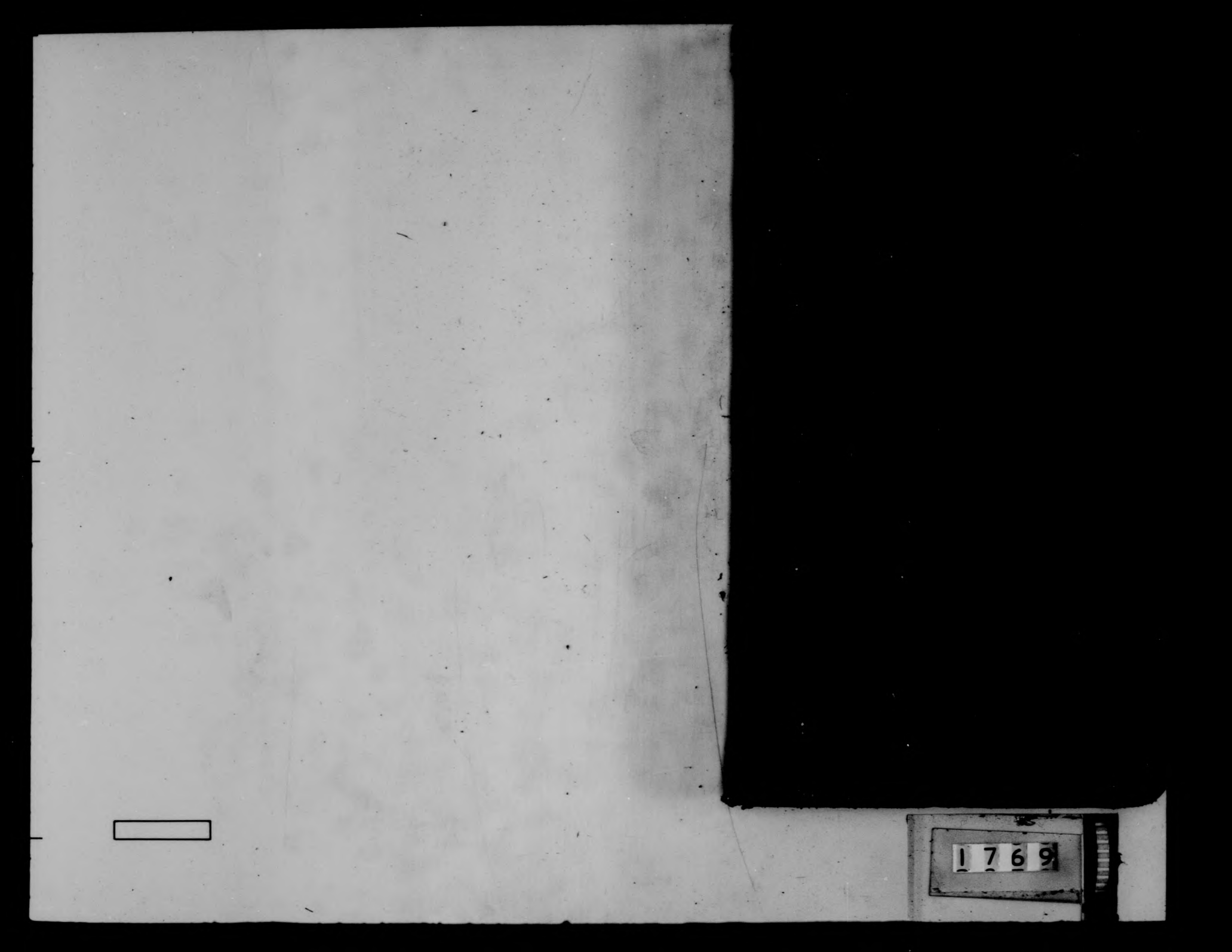

1769

No. 93441
THIS BOOK WAS MADE BY
The Hicks-Judd Co.
Printers and Blank Bookbinders
73 First St. San Francisco.
Give above number, when ordering

50464

INDEX

1770

C.E. Dippletf

1116 14th between K & L

See pg. 14.

Notes 1 - 14 (2)
14 — Duplicate

1771

1584 0584 1683 0584 1679 0584 1683 0584 1684 0584 Site Field Sheet

0011 9047

1772

00119047

1773

Sta. 504 Elev. Grade.

0.0119047

0.0119047

See Book of "Original X Sections, Sta. 360 to 504".

1774

"E" Elev Grade

See Book of "Original X Sections, Sta. 360 to 504".

1775

Elevations Grade.

-0.0119047

473+21.5 Bent No 6

Sec Pipe To-

472+47.5 Bent No 5

6 Bent Pile opening - 5 Spans

-0.0119047

See Book of "Original X Sections, Sta. 360 to 504".

1776

Elevation Grade

+90 6.2 26.644 0.0119047 26.655 26.673

+60 6.3 26.648 26.661 26.667

+30 6.5 26.651 26.684 26.688

479 1.45 6.5 26.678 26.691 26.695

+60 3.00 6.8 26.661 26.684 26.688

+30 6.5 26.667 26.691 26.695

+90 6.8 26.688 26.691 26.698

+60 6.3 0.0119047 26.695 26.698

+30 7.4 26.698 26.698 26.702

475

Grading Cottonwood Tree.

See Book of "Original X Sections, Sta. 360 to 504".

1777

"E"

Foundation Finish

483+79 Bent No 12

13 Bent Pile Opening - 12 Spans

See Page 70

0.0119047

483+84.5

483+84.5

483+79

483+63

483+45

483+26

483+07

482+88

482+69

482+50 - Bent No. 1

482+31

482+12

482+00

481+81

481+60

481+41

481+20

0.0119047

N 25° W

26.6637 E.C.20

26.6641

Grading small Basswood Tree

Hub near Edge of 2nd Bench

Hub near 2nd Bench

Hub near Edge of 2nd Bench

Hub near 2nd Bench

Hub near Edge of 2nd Bench

Hub near 2nd Bench

See Book of "Original" Sections, Sta. 360 to 504.

1779

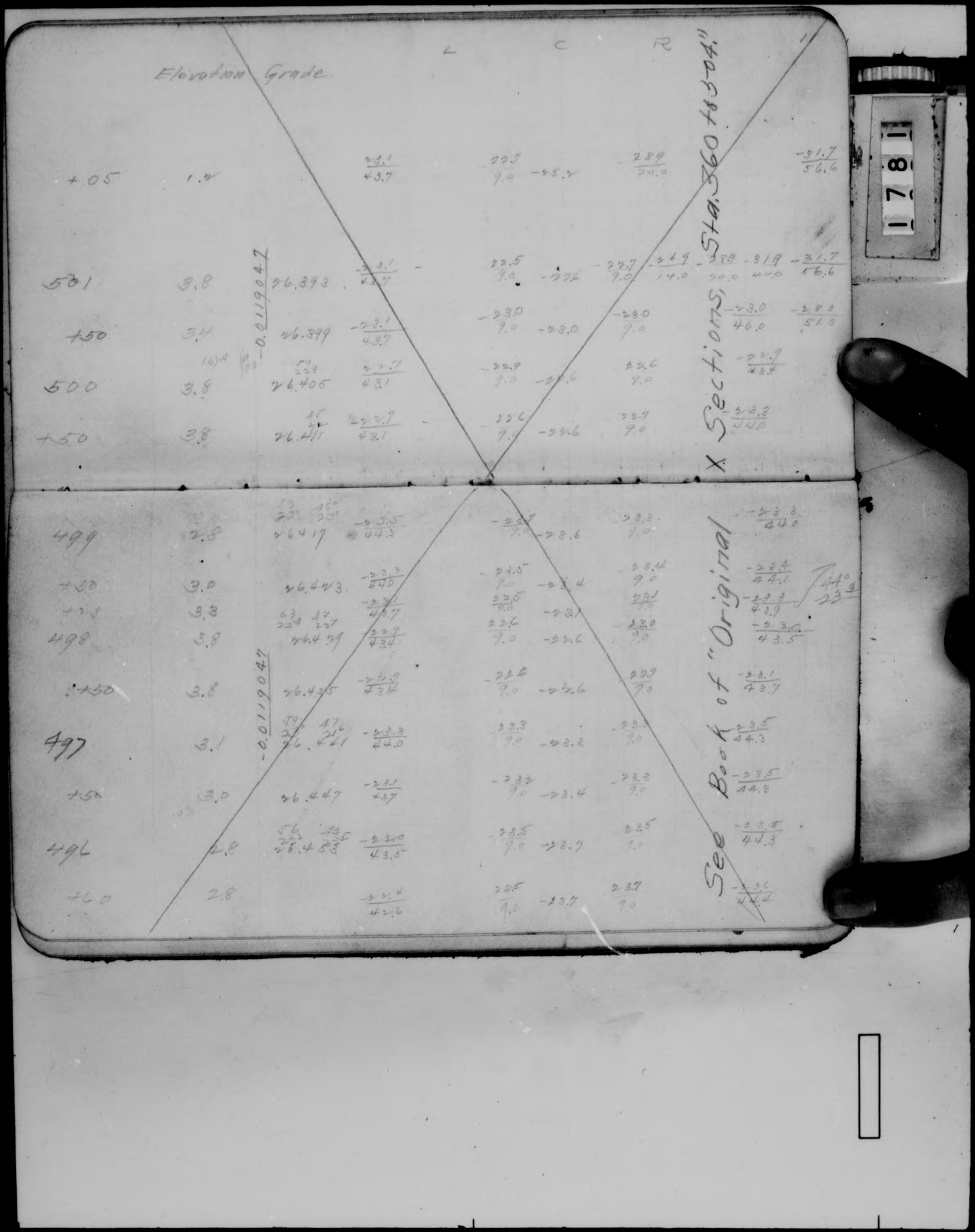
Elevation Grade

-0.0119047

-0.0119047

See Book of "Original Sections, Sta 360 to 504".

1780


L C R
Elevation Grade
+05 1.4
501 3.8 26.393
+50 3.4 26.399
500 3.8 26.405
+50 3.8 26.411
499 2.8 26.417
+50 3.0 26.423
+75 3.3
498 3.8 26.439
+50 3.8 26.435
497 3.1 26.441
+50 3.0 26.447
496 2.8 26.453
+50 2.8
-0.011904Z
-0.011904Z
X Sections, Sta. 360 to 304"
See Book of "Original"

Elev Grade

503

-1.3

+3.0

-7.7

-0.0119047

-7.2

Out Dist.

12

501 +30

-2.8

-0.0119047

See Book of "Original X Sections" Stg. 360 to 504".

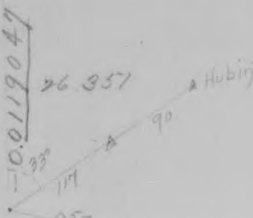
1782

'E' Elev Grade

500	17.7	76.345		-5.8 / 17.7	-6.8 / 9.0	-8.6	-11.0 / 9.0	-20.8 / 40.2
+50	19.5	76.357	Hubing Tules	-7.0 / 19.5	-8.7 / 9.0	-6.9	-8.4 / 9.0	-14.8 / 30.0
501+26.5 Point on tangent								
504	20.0	76.357		-13.7 / 28.8	-	-8.2 / 9	-6.4	-6.4 / 9.0	-8.5 / 21.7

-0.011904?

July 12th 1905

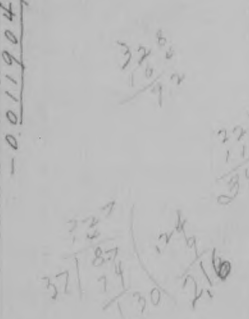


503+50	12.4	76.363	63 / 16.1 / -33.7 / 57.3	-32.8 / 45.0	-22.7 / 37.0	-18.0	-13.1 / .9	-9.7 / 23.6

9 / 16.1

37'

-0.011904?



"I"	Elev.	Grade	
+50	15.9	26.291	16.7 14.9 9.0 -10.4 9.0 1.9 2.9 3.89 -5.1 -7.2 -7.8 -12.9 -16.3 -18.2 -19.2
509	17.5	26.297	15.3 13 9.0 -8.8 9.0 3.6 3.1 3.96 -4.2 -6.7 -7.2 -17.4 -18.2 -18.3 -20 -20.1
+50	17.4	26.303	14.7 9.0 -8.2 9.0 1.9 2.9 3.93 -3.8 -5.1 -11.4 -13.2 -14.7 -18.3 -20.3
508	17.7	26.309	-8.5 -4.7 -6.8 -8.6 -10.6 -20.8 -20.8 13.0 9.0 9.0 29.0 40.7 16'
+50	16.6	26.315	-10.0 -4.8 -7.6 -9.7 -12.6 -20.4 16.2 9.0 9.0 39.6
507	17.1	26.321	-9.5 -4.0 -6.2 -9.2 -14.2 -21.6 15.0 9.0 9.0 37.0 41.6
+70	15.0	26.324	-11.6 -6.2 -7.5 -11.3 -14.9 -21.6 13.3 9.0 9.0 32.0 41.4
+50	16.4	26.327	-10.3 -5.9 -8.4 -9.9 -13.2 -21.6 -21.8 17.8 9.0 9.0 27.0 41.7 17.9
506	16.1	26.333	-10.4 -6.6 -8.8 -10.2 -13.2 -21.2 -21.2 16.9 9.0 9.0 29.0 40.8
505 +50	17.1	26.339	-9.4 -6.6 -7.7 -9.2 -13.6 -20.6 -21.0 15.9 9.0 9.0 28.0 40.5

Duplicate of Mayor Holes

11784

"E"	Elev.	Grade								
+50	16.1	26.238	16.4 -4.9	9.0 -8.2	-10.1	9.0 -13.2	19 -15.1	29 -17.4	35.4 -17.9	
514	15.9	26.288	15.9 -4.2	9.0 -7.3	-10.3	9.0 -12.6	19 -13.2	24.5 -15.1	29 -17.1	33.3 -17.4	35.1 -17.6
+50	15.3	26.344	16.5 -5.0	9.0 -7.2	-10.9	9.0 -13.9	19 -16.0	24 -17.2	29 -17.2	34.7 -17.4	35.1 -17.4
513	17.7	26.350	17.3 -5.5	9.0 -7.2	-8.5	9.0 -13.7	16 -14.6	19 -15.5	21 -17.0	29 -17.2	34.4 -17.0
+50	17.0	26.356	17.3 -5.5	9.0 -7.2	-9.9	9.0 -13.3	19 -15.3	24 -15.6	29 -17.5	35.6 -17.6	
512	17.3	26.362	17.4 -5.6	9.0 -7.2	-9.0	9.0 -10.3	19 -14.9	24 -15.5	29 -17.2	35.3 -17.5	
+50	16.6	26.368	16.6 -4.7	9.0 -6.7	-9.7	9.0 -12.2	19 -14.3	29 -17.1	34.7 -17.2		
511	16.2	26.374	16.2 -4.3	9.0 -7.3	-10.1	9.0 -12.2	19 -14.1	29 -16.3	35.4 -17.6		
+50	16.6	26.380	15.2 -4.2	9.0 -7.5	-9.7	9.0 -13.3	19 -15.7	25 -17.6	29 -17.6	35.4 -17.6	
510	15.4	26.386	16.3 -5.3	9.0 -7.3	-10.9	9.0 -12.8	19 -15.8	24 -17	36.0 -18.0		

0.011904 7

0.011904 7

17851

"F"	F lev	Grade								
+50	18.1	26.172	-3.0 / 13.5	-3.5 / 7.0	-8.1	9.0 / -12.6	19 / -16.3	29 / -18.4	39 / -20.2	49 / -20.9
			13.8 / -5.2	9.0 / -3.7						
519	17.6	26.178	-3.9 / 18.2	-4.2 / 7.0	-8.6	9.0 / -12.4	19 / -15.6	29 / -19.2	38.9 / -19.2	
			13.4 / -3.9	9.0 / -4.2						
+50	18.1	26.184	-4.0 / 15.0	-5.7 / 9.0	-8.1	9.0 / -12.6	19.0 / -14.6	29 / -17.2	38.9 / -19.5	
			15.9 / -4.9	9.0 / -5.5						
518	15.4	26.190	15.6 / -5.9	9.0 / -7.2	-10.8	9.0 / -12.6	19 / -14.8	29 / -17.6	36.8 / -18.5	
+50	16.7	26.196	14.3 / -3.5	9.0 / -5.0	-9.5	9.0 / -12.8	19 / -15.4	29 / -17.1	35.9 / -17.9	
517	18.1	26.202	14.0 / -3.9	9.0 / -4.6	-8.1	9.0 / -10.5	19 / -14.1	29 / -17.2	38.2 / -19.9	
+87			13.7 / -4.1	9.0 / -6.2	-9.4	9.0 / -11.8	19 / -14.9	29 / -18.1	37 / -19.5	39.3 / -20.7
+50	16.2	26.208	15.6 / -4.4	9.0 / -5.6	8.0 / -9.0	-10.0	9.0 / -12.1	19 / -14.7	29 / -17.9	36 / -18.9
516	17.0	26.214	14.7 / -3.8	9.0 / -4.8	-9.2	9.0 / -12.4	19 / -13.9	29 / -17.0	34 / -20.2	39.7 / -20.4
+50	16.3	26.220	12.9 / -2.6	9.0 / -4.2	-9.9	9.0 / -13.4	19 / -16.5	29 / -17.4	35.7 / -17.9	
515	16.8	26.226	-4.2 / -15.9	-7.9 / 9.0	-9.4	9.0 / -11.4	11 / -13.0	19 / -14.5	29 / -17.2	38.1 / -19.4

-0.011904?

-0.011904?

17869

Allen Miller 17

"E"	Elev.	Grade							
+50	19.3	26.113	-3.6 / 13.5	-2.8 / 9.0	-6.8	90 -9.6	190 -11.8	29 -16.8	37 -19.1	378 -19.2
			13.5	9.0						
			-3.0	-2.8						
528	20.7	26.119	-3.8 / 12.7	-2.6 / 9.0	-5.4	90 -7.8	190 -12.5	29.0 -16.0	357 -17.6	
			12.6	9.0						
			-2.6	-2.6						
-50	20.5	26.125	-2.6 / 12.9	-2.1 / 9.0	-5.6	90 -9.2	19 -13.7	29 -16.8	375 -19.0	
			13.1	9.0						
			-2.7	-2.6						
523	20.8	26.121	-3.0 / 13.8	-2.2 / 9.0	-5.3	90 -9.1	19 -12.0	29 -17.6	384 -19.6	
			12.8	9.0						
			-2.6	-3.3						
+50	21.4	26.137	-2.4 / 12.6	-2.6 / 9.0	-4.7	90 -10.3	18 -12.7	19 -15.5	29 -19.7	39 -21.5	408 -21.2
			12.3	9.0						
			-2.2	-2.2						
527	19.8	26.143	-3.4 / 14.1	-2.7 / 9.0	-6.3	90 -10.5	190 -13.8	29 -17.6	39 -19.8	387 -19.8
			36	2.0	4.8					
			-1.4	-2.8	10.5					
+50	19.9	26.149	-5.0 / 16.5	-3.8 / 9.0	-6.3	90 -11.3	190 -14.3	29 -16.4	377 -19.1	
			17.3	9.0						
			5.5	-4.1						
521	21.2	26.155	-4.0 / 15.0	-3.4 / 9.0	-5.0	90 -10.6	19 -13.5	29 -17.2	389 -19.0	
			12.3	9.0	5.1					
			-2.3	-2.1	-2.0					
+50	19.1	26.161	-4.7 / 15.3	-3.3 / 9.0	-7.1	90 -11.7	19 -15.5	29 -19.6	396 -20.2	
			15.6	9.0						
			-4.4	-3.3						
520	17.3	26.167	-3.8 / 14.7	-4.1 / 9.0	-8.9	-12.4 / 9.0	-20.0 / 34	-29.6 / 39.7		
			15.3	9.0		90 -12.3	19.2 -15.7	29 -19.2	39 -21.3	46.7 -21.1
			4.7	-4.2						

17871

"E"	Elev	Grade	
530	14.0	26.047	
+50	13.2	26.053	
529	13.3	26.059	
+50	12.7	26.065	-.0011984
528	16.6	26.071	
+50	17.4	26.077	
527	16.9	26.083	
+50	15.3	26.089	-.0011984
526	16.9	26.095	
+12	17.3	26.101	
525	18.7	26.107	

1788

17869

	+50	16.4	25.981	24[4]	22	19	9	9	9	19	29	36
				-13[6]	-10[3]	-9[2]	-7	-9[6]	-12[3]	-13[3]	-15[9]	-18[3]
V35		15.0	25.987	26[3]	24	19	9	9	9	19	29	32
				-11[5]	-12[6]	-9[8]	-10[7]	-11[3]	-12[2]	-13[1]	-15[1]	-18[2]
	+50	14.0	25.993	28[5]	19	9	9	19	29	36
				-13[2]	-16[4]	-11[5]	-12[2]	-13[2]	-14[7]	-16[6]	-18[4]	
V34		13.9	26.004	27[6]	19	9	9	19	29	36
				-12[7]	-15[2]	-11[2]	-12[1]	-13[8]	-15[4]	-16[3]	-18[2]	
	+50	13.6	26.005	30	19	9	9	19	29	36
				-13[3]	-13[1]	-13[6]	-12[4]	-13[7]	-14[2]	-16[2]	-18[2]	
V33		13.5	26.011	28[5]	19	9	9	19	29	36
				-[7]	-11[7]	-11[2]	-12[5]	-14[1]	-15[3]	-17[4]	-18[1]	
	+50	13.7	26.017	27[9]	19	9	9	19	29	35
				-12[6]	-12[0]	-11[6]	-13[8]	-13[9]	-15[3]	-16[7]	-17[7]	
V32		13.4	26.023	27[1]	19	9	9	19	29	39
				-13[2]	-11[6]	-11[3]	-12[6]	-13[9]	-15[2]	-18[3]	-20[1]	
	+50	13.6	26.029	25[1]	19	9	9	19	29	38
				-12[7]	-11[4]	-12[1]	-12[4]	-14[1]	-15[6]	-17[2]	-19[9]	
V31		14.7	26.035	27[3]		9	9	19	29	39
				-13[4]		-12[0]	-11[2]	-13[5]	-15[3]	-17[3]	-20[3]	
	+50	13.9	26.041	26		9	9	19	29	39	40
				-11[3]		-10[7]	-12[4]	-13[1]	-15[3]	-17[2]	-20[5]	-21

1790

	+50	~~16.5~~ 15.9	25 935 157	25^{7} 23^{3} 19 9 9 19 29 38^{1} -12^{8} -11^{7} -9^{7} $-8^{4\frac{1}{2}}$ -10^{0} -12^{1} $-15^{2\frac{1}{2}}$ -18^{4} -19^{9}
√39		~~16.3~~ 15.1	25 941 158	25^{5} 19 9 19 29 39 42^{5} -12^{7} -10^{3} -9^{5} -10^{1} -12^{5} -16^{2} -19^{5} -21^{9} -23^{5}
	+50	16.7	25 947	20^{9} 19 9 9 19 29 35^{0} -7^{6} -9^{9} -8^{5} -9^{3} -10^{6} -13^{7} -15^{6} -17^{2}
√38		16.8	25 953	23^{3} 19 9 9 19 29 30^{3} -9^{5} -8^{2} -8^{3} -9^{2} -9^{6} -12^{9} -13^{9} -14^{2}
	+50	15.8	25 958	22^{6} 19 9 9 19 29 32^{7} -10^{2} -8^{9} -9^{2} -10^{2} -9^{9} -13^{2} -15^{1} -15^{7}
√37		16.5	26 005	25^{5} 19 9 9 19 29 (33^{4}) -11^{0} -9^{9} -8^{8} -9^{5} -10^{8} -12^{8} -15^{4} -16^{4}
	+50	16.0	26 011	26^{9} 19^{8} 9^{2} 9 19 29 (36^{9}) -11^{9} -9^{7} -9^{2} -10^{0} -11^{8} -14^{7} -15^{6} -18^{2}
√36		15.7	26 016	25^{7} 21 19 9 9 19 29 (36^{9}) -11^{2} -10^{1} -9^{3} -8^{7} -10^{3} -12^{2} -14^{0} -15^{3} -18^{0}

1791

Sta		Elev	Grade								
	+50	12.6	25.9	20.6	9	9	19	29	39	43.1
				-7.7	-11.0	-13.3	-15.1	-18.7	-21.8	-22.6	-22.9
SA6		17.0	25.9	20.9	18	9	19	29	39	43.7
				-7.9	-10.0	-10.0	-15.6	-19.0	-20.3	-22.7	-23.1
	+50	14.5	25.9	21.6	9	9	19	29	39	43.7
				-8.1	-9.6	-11.4	-14.7	-17.5	-20.8	-22.5	-23.1
SA5		17.3	25.9	21.3	19	9	19	29	39	42.9
				-8.1	-10.1	-12.0	-13.6	-16.8	-19.4	-22.3	-22.6
	+50	13.0	25.9	21	9.0	9	19	29	38	
				-8.0	-11.2	-12.9	-15.4	-17.8	-18.6	-19.3	
SA4		14.9	25.9	20.4	9	9	19	29	39.5	
				-7.6	-9.0	-11.0	-14.2	-17.4	-18.7	-20.3	
	+50	15.3	25.9	21	9	9	19	29	38.0	
				-8.0	-8.1	-10.6	-13.5	-16.3	-17.9	-19.9	
SA3		15.5	25.9	20.7	9	9	19	29	38.0	
				-7.8	-8.5	-10.4	-14.0	-15.6	-16.4	-19.3	

Sta		Elev	Grade	
	+36	12.7	25.8	
J47	+06	12.0	25.8	
	+76	13.4	25.8	
	+16	13.9	25.8	
J48	+16	13.7	25.8	⊙ B.S.
J48		13.2	25.8	
	+50	12.9	25.8	
J47		12.8	25.8	

1793

Sta		Elev	Grade	
13+39.64	+50	64	25.0	

Feb 6

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Jan 30

Jan 31

Feb 1

Feb 2

Feb 3

Feb 4

Feb 5

S 19

V5-8

		Fin. Grade
		25'
1+65'		
		25' 0 E.C.
V7 + 24.1	14	
		25' 01
1+98'		
		25' 02
1+64'		
		25' 0'
1+34'		
		25' 0'
V56 + 04'	13'	
		25' 0'
1+74'		
		25' 03
1+41'		
		25' 0'

26

1796

	Elev	Grade
+ 17.5	19.8	
+ 50	15.9	
1342		
	17.3	
+ 846	18.2	
+50	19.2	

- 0.0022'

1341	20.3	
-		
+ 50	21.9	
1340	21.3	

- 0.0022'

BM On Sycamore 80' N 1326+35' Elev. = 16.32'

1797

		Elev. Grade
+50		187
1346		184
	+50	21.0
	+33	21.6
1345		22.0

-0.0022+

	+50	22.1
1344		22.0
	+50	21.5
1343		196

-0.0022+

28

1798

+80	19.1	13.47							
+50	18.0	13.48							
+50	15.6	13.48							
	15.2	12.48							
+50	14.8	13.49							
+50	12.4	13.49							

-0.00.22+

Elev. at pole

29

1799

1350	11.3	+50
1351	11.4	+50
1352	10.4	+50
	9.8	+50
	9.3	+50
Elev. Grade	10.1	+65

-0.00222

30

1800

	Elev	Grade
+ 25	11.5	2|6
1355	10.6	2|6
+ 50	10.7	2|6
1354	10.0	2|6

-0.002'

+ 30	9.0	2|6
+ 22.4	9.8	2|6
+ 05	14.6	2|6
1353	14.8	2|6
+ 80	14.7	2|6

2\|6 BC 30'2

1801

	Elev	Grade		Left		C	Right			
+ 50	9.4	21.6		-12.6 (27.9)	-12.4 (9)	-12.2	-9.9 (9)	-5.9 (17.1)	-2.2 (23)	Levee
1357	10.1	21.6	-0.0022	-12.5 (29.8)	-12.0 (9)	-11.5	-7.7 (9)	-4.2 (15.3)	-2.1 (18.0)	Levee
+ 50	12.3	21.6	End of new Levee	-15.2 (31.8)	-14.6 (9)	-9.3	-4.3 (9)	-2.6 (13.9)	-1.8 (15)	
+ 20	13.7	21.6								
+ 15	15.4	21.6								
+ 05	16.1	21.6								
1356	16.9	21.6								
+ 9.5	18.3	21.6								
+ 8.5	18.2	21.6								
+ 80	15.8	21.6								
+ 65	11.6	21.6								
+ 50	11.0	21.6								

See Transit Book #4, page 9.
See Level Book #8, page 9

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Final Estimate No. 197

Left C Right

Nail in Tree 122° Hub at base of Tree 74' N.68 E. Mag.

	E Lev.	Grade								
+63	8.9	21.6	BC. 45° R			-12.7				
			140'							
+50	9.1	21.6		-12.8 (28.2)	-12.5 (9)	-12.5	-10.6 (9)	-5.9 (17.9)	-2.6 (23.0)	Levee
			Hub at base of Tree							
			146' N.33 W. mag							
			Nail in Tree							
1360	9.8	21.630	X	-13.4 (29.1)	-12.7 (9)	-11.8	-9.9 (9)	-6.9 (19.4)	-3.1 (25.0)	Levee
+50	9.1	21.6		-12.8 (28.2)	-12.5 (9)	-12.5	-11.3 (9)	-7.8 (20.5)	-3.9 (26.0)	Levee

-0.014

-0.0022'

1359	8.8	21.6		-12.9 (28.4)	-12.6 (9)	-12.8	-12.8 (9)	-7.6 (20.4)	-3.9 (26)	Levee

Nail in Tree 112½ 60.5 E Mag. Hub at base of Tree on W Side Sunk .4' 10e.

+96	8.4	21.6	E C			-13.2				

97.3 N 21.8 W Mag

149 Hub at root of Small Tree .4' below surface

Nail in Tree

+50	9.0	21.6		-13.1 (28.7)	-12.8 (9)	-12.6	-10.9 (9)	-6.4 (18.6)	-2.3 (25)	Levee
1358	9.2	21.6		-12.8 (28.2)	-12.4 (9)	-12.4	-8.3 (9)	-4.6 (13.9)	-1.2 (21)	Levee

1803

Left ℄ Right

	Elev.	Grade						
+85	15.0	21.6			-6.6			
+50	12.6	21.6	$-\frac{12.3}{27.3}$	$-\frac{11.6}{9}$	-9.0	$-\frac{3.9}{9}$	$-\frac{2.5}{17.8}$	$-\frac{2.5}{12.8}$
1363	10.6	21.6	$-\frac{12.8}{28.2}$	$-\frac{12.8}{9}$	-11.0	$-\frac{11.3}{9}$	$\frac{2.5}{11.5}$	$-\frac{2.2}{12.3}$
					-9.1			
+75	12.5	21.6						
+50	11.5	21.6	$-\frac{11.9}{26.9}$	$-\frac{11.5}{9}$	-10.1	$-\frac{11.21}{9}$	$-\frac{2.2}{12.3}$	$-\frac{1.6}{14.1}$ Levee
1362	11.7	21.6	$\frac{12.8}{28.5}$	$-\frac{11.3}{9}$	-9.9	$-\frac{6.4}{9}$	$\frac{3.2}{13.8}$	$\frac{1.9}{16}$ Levee
+50	10.9	21.6	$-\frac{12.4}{27.8}$	$-\frac{11.6}{9}$	-10.7	$-\frac{7.5}{9}$	$-\frac{4.1}{15.2}$	$-\frac{2.2}{18.5}$ Levee
1361	9.4	21.6	$-\frac{12.8}{28.2}$	$-\frac{12.3}{9}$	-12.2	$-\frac{9.5}{9}$	$-\frac{5.3}{17.0}$	$-\frac{2.7}{21.5}$ Levee

-0.014

1804

Left c Right

	Elev	Grade		
B.M. 1366	17.875	21.5	60 ft. R. on Eucalyptus.	
+ 50	10.7	21.6	-0.014	$-\frac{11.7}{25.7}$ $-\frac{11.7}{9}$ -10.9 $-\frac{7.3}{9}$ $-\frac{3.9}{14.9}$ $-\frac{2.9}{16.0}$ Levee
1365	13.7	21.6		$-\frac{11.2}{25.8}$ $-\frac{10.7}{9}$ -7.9 $-\frac{3.6}{9}$ $-\frac{3.0}{11}$ $-\frac{2.7}{13.1}$
+ 85	14.5	21.6		$\frac{10.1}{24.2}$ $\frac{8.7}{9}$ -7.1 $-\frac{3.1}{9}$ $\frac{2.7}{13.1}$
+ 80	16.7	21.6 △		$-\frac{9.1}{22.9}$ $-\frac{7.3}{9}$ -4.9 $-\frac{3.1}{9}$ $-\frac{2.7}{13.1}$
+ 68.2 △		21.6 △		
+ 65	16.6	21.6		$-\frac{7.8}{20.11}$ $-\frac{5.9}{9}$ -5.0 $-\frac{3.2}{9}$ $-\frac{2.8}{13.2}$
+ 50	17.3	21.6		$-\frac{9.7}{23.0}$ $-\frac{9.7}{9}$ -7.3 $-\frac{2.6}{9}$ $-\frac{2.4}{12.6}$
+ 20	15.8	21.6		-5.8 $\frac{1.5}{9}$
+ 10	13.5	21.6		-8.1
1364	13.3	21.6		$-\frac{11.2}{26.1}$ $-\frac{11.1}{9}$ -8.3 $\frac{2.3}{9}$ $\frac{3.0}{13.5}$

1805

	Elev	Grade	Left	℄	Right
1369	12.2	21.5	$-\frac{12.5}{2.78}$ $-\frac{12.0}{9}$	-9.3	$-\frac{5.0}{9}$ $-\frac{2.7}{13.1}$ $-\frac{1.2}{16}$ Levee
+50	11.3	21.5	$-\frac{11.9}{26.9}$ $-\frac{11.9}{9}$	-10.2	$-\frac{6.4}{9}$ $-\frac{3.2}{13.8}$ $-\frac{1.6}{16.0}$ Levee
1368	10.8	21.5	$-\frac{12.9}{28.4}$ $-\frac{12.9}{9}$	-10.7	$-\frac{7.2}{9}$ $-\frac{4.3}{13.0}$ $-\frac{2.0}{17}$ Levee
+50	10.7	21.5	$-\frac{12.7}{28.1}$ $-\frac{12.7}{9}$	-10.8	$-\frac{6.0}{9}$ $-\frac{3.0}{13.5}$ $-\frac{2.0}{14.5}$ Levee
1367	10.4	21.5	$-\frac{12.7}{28.1}$ $-\frac{12.7}{9}$	-11.1	$-\frac{8.9}{9}$ $-\frac{4.7}{16.1}$ $-\frac{2.6}{18.5}$ Levee
+50	11.0	21.5	$\frac{12.1}{27.2}$ $-\frac{12.3}{9}$	-10.5	$-\frac{8.1}{9}$ $-\frac{4.4}{15.6}$ $-\frac{2.6}{18.0}$ Levee
1366	9.3	21.5	$-\frac{12.9}{28.4}$ $-\frac{12.9}{9}$	-12.2	$-\frac{8.8}{9}$ $-\frac{4.3}{15.5}$ $-\frac{2.8}{18}$ Levee

-2.014

1806

	Elev.	Grade	Left	c	Right
+50	10.1	21.5	$-\frac{13.7}{28.2}$	$-\frac{12.3}{9}$ -11.4	$-\frac{7.4}{9}$ $-\frac{3.9}{14.9}$ $-\frac{1.5}{18.0}$ Levee
1372	10.1	21.5	$\frac{15.5}{28.1}$	$\frac{12.7}{9}$ -11.41	$-\frac{9.3}{9}$ $-\frac{5.0}{16.5}$ $-\frac{2.7}{19}$ Levee
+50	9.9	21.5	$-\frac{12.9}{28.1}$	$-\frac{13.0}{9}$ -11.6	$-\frac{9.1}{9}$ $-\frac{4.6}{15.9}$ $-\frac{1.8}{19.5}$ Levee
1371	10.3	21.5	$-\frac{13.1}{28.3}$	$-\frac{13.1}{9}$ -11.2	$-\frac{7.4}{9}$ $-\frac{3.7}{14.6}$ $-\frac{1.8}{17.5}$ Levee
+50	10.7	21.5	$-\frac{12.8}{28.2}$	$-\frac{13.0}{9}$ -10.8	$-\frac{7.2}{9}$ $-\frac{3.7}{14.6}$ $-\frac{2.1}{17}$ Levee
△1370	10.2	21.5 △	$\frac{12.2}{27.3}$	$-\frac{12.6}{9}$ -10.3	$-\frac{8.2}{9}$ $-\frac{4.2}{15.3}$ $-\frac{1.9}{18.0}$ Levee
+50	10.8	21.5	$-\frac{12.6}{27.9}$	$-\frac{12.3}{9}$ -10.7	$-\frac{8.0}{9}$ $-\frac{4.2}{15.3}$ $-\frac{2.2}{18.0}$ Levee

-0.014

18071

	Elev.	Grade	Left			℄		Right		
+65	13.2	21.4								
			$-\frac{11.6}{26.4}$	$-\frac{10.9}{9}$	-8.2		$-\frac{2.0}{9}$	$-\frac{2.0}{12}$		
+50	18.6	21.4								
			$-\frac{8.1}{21.2}$	$-\frac{7.6}{19}$	$-\frac{4.9}{9}$	-2.8	$-\frac{2.1}{9}$	$-\frac{1.9}{11.9}$		
+05	18.4	21.4								
			$-\frac{7.8}{20.9}$	$-\frac{4.3}{9}$	-3.0		$-\frac{1.3}{9}$	$\frac{1.1}{10.9}$		
1375	16.7	21.4								
			$-\frac{11.3}{25.8}$	$-\frac{6.5}{9}$	-4.7		$-\frac{1.8}{9}$	$\frac{1.3}{11.8}$		
+75	9.1	21.4								
			$-\frac{11.5}{26.3}$	$-\frac{12.0}{9}$	-12.3		$-\frac{11.3}{9}$	$-\frac{6.0}{16.0}$	$-\frac{1.3}{26.0}$	Levee
+50 △	8.44	21.4								
			$\frac{12.7}{28.1}$	$-\frac{12.7}{9}$	-13.0		$-\frac{12.1}{9}$	$\frac{7.0}{19.5}$	$\frac{1.5}{20}$	Levee
1374	10.0	21.4								
			$-\frac{12.8}{28.3}$	$-\frac{12.8}{19}$	$-\frac{11.5}{9}$	-11.4	$-\frac{8.8}{9}$	$-\frac{4.9}{16.4}$	$-\frac{1.3}{23}$	Levee
+50	10.3	21.4								
			$-\frac{12.7}{28.1}$	$-\frac{11.5}{9}$	-11.1		$-\frac{8.0}{9}$	$-\frac{4.5}{15.8}$	$-\frac{1.3}{20}$	Levee
1373	10.3	21.5								
			$-\frac{12.9}{28.2}$	$-\frac{12.9}{9}$	-11.2		$-\frac{7.41}{9}$	$-\frac{3.6}{11.4}$	$\frac{1.9}{18}$	Levee

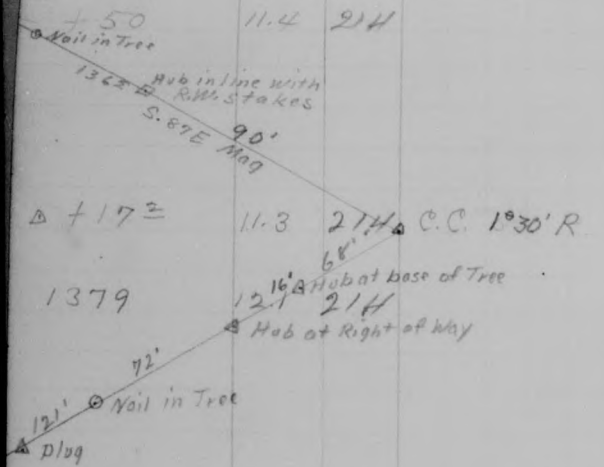
-0.014

1808

	Elev.	Grade	Left	C.	Right
1378	12.0	21.4	$-\frac{12.6}{27.9}$ $-\frac{11.5}{9}$	-9.4	$-\frac{2.6}{9}$ $-\frac{2.3}{11.5}$ $-\frac{2.3}{12.5}$ Levee
			-0.014		
A + 812	11.55	21.4 △	$\frac{12.9}{28.4}$ $-\frac{11.5}{9}$	-9.8	$-\frac{2.8}{9}$ $-\frac{2.3}{10}$ $-\frac{2.1}{12.2}$ Levee
+ 50	12.0	21.4	$-\frac{13.1}{28.4}$ $-\frac{11.7}{9}$	-9.4	$-\frac{2.5}{9}$ $-\frac{2.3}{9.5}$ $-\frac{2.1}{12.2}$ Levee
B.M.	17.821	21.4	On stump 60 ft. R of 1378.		
1377	14.9	21.4	$-\frac{13.0}{24.5}$ $-\frac{11.0}{19}$ $-\frac{10.5}{9}$	-6.5	$-\frac{.6}{7.5}$ $-\frac{.6}{9}$ $-\frac{.6}{9.9}$
+ 50	14.4	21.4	$-\frac{12.5}{24.5}$ $-\frac{10.3}{9}$	-7.0	$-\frac{1.9}{8}$ $-\frac{1.9}{9}$ $-\frac{1.3}{11.8}$
1376	14.3	21.4	$-\frac{11.3}{24.0}$ $-\frac{19.1}{19}$ $-\frac{10.2}{9}$	-7.1	$-\frac{1.0}{9}$ $-\frac{.8}{10.3}$

1806

	Elev.	Grade	Left	℄	Right
1381	10.0	21.3	$-\frac{13.4}{29.1}$ $-\frac{12.8}{9}$ -11.3		$-\frac{6.7}{9}$ $-\frac{3.2}{13.4}$ $-\frac{2.6}{15}$ Levee
+50	12.2	21.3	$-\frac{12.4}{29.0}$ $-\frac{10.5}{9}$ -9.1		$\frac{4.4}{9}$ $\frac{2.2}{12.3}$ $\frac{1.7}{13.0}$ Levee
1380	11.9	21.4	$-\frac{12.9}{28.4}$ $-\frac{10.7}{9}$ -9.5		$\frac{4.9}{9}$ $\frac{2.0}{12.0}$ Levee
+50	11.4	21.4	$-\frac{12.7}{28.1}$ $-\frac{9.8}{9}$ -10.0		$\frac{4.4}{9}$ $\frac{2.1}{12.2}$ Levee
△ +17.2	11.3	21.4	△ C.C. 1°30' R $-\frac{13.2}{29.0}$ $-\frac{10.7}{9}$ -10.1		$-\frac{3.9}{9}$ $-\frac{2.2}{12.3}$ Levee
1379	12.1	21.4	$-\frac{12.9}{28.4}$ $-\frac{10.5}{9}$ -9.3		$-\frac{3.8}{9}$ $-\frac{2.1}{11.9}$ $-\frac{2.1}{12.2}$ Levee
+50	13.3	21.4	$-\frac{14.0}{30.0}$ $\frac{11.0}{9}$ -8.1		$-\frac{2.5}{9}$ $\frac{2.3}{9.5}$ $\frac{2.1}{12.2}$ Levee



1810

	Elev.	Grade	Left									Center	Right								
+50	10.5	21.3																			
			$-\frac{12.9}{28.4}$	$-\frac{12.5}{9}$	-10.8	$-\frac{10.8}{6}$	$-\frac{8.7}{9}$	$-\frac{4.4}{15.6}$	$-\frac{2.9}{19}$	Levee											
1384	10.1	21.3																			
			$-\frac{13.2}{28.8}$	$-\frac{12.8}{9}$	-11.2	$-\frac{11.2}{6}$	$-\frac{9.8}{9}$	$-\frac{5.1}{16.7}$	$-\frac{3.3}{19.5}$	Levee											
+50	10.2	21.3																			
			$-\frac{13.4}{29.1}$	$-\frac{12.9}{9}$	-11.1	$-\frac{10.5}{6}$	$-\frac{9.6}{9}$	$-\frac{5.0}{16.5}$	$-\frac{3.1}{19.2}$	Levee											
1383	9.9	21.3																			
			$-\frac{13.2}{29.8}$	$-\frac{12.9}{9}$	-11.4	$-\frac{11.4}{4}$	$-\frac{8.7}{9}$	$-\frac{4.6}{15.9}$	$-\frac{3.2}{18}$	Levee											
+50	9.4	21.3																			
			$-\frac{13.2}{28.9}$	$-\frac{12.4}{9}$	-11.9	$-\frac{7.8}{9}$	$-\frac{3.7}{14.4}$	$-\frac{2.3}{16.5}$	Levee												
1382	10.2	21.3																			
			$-\frac{12.9}{28.4}$	$-\frac{12.6}{9}$	-11.1	$-\frac{6.8}{9}$	$-\frac{3.6}{14.9}$	$-\frac{1.8}{17}$	Levee												
+50	9.2	21.3																			
			$-\frac{12.7}{28.1}$	$-\frac{12.7}{9}$	-12.1	$-\frac{8.1}{9}$	$-\frac{4.1}{15.2}$	$-\frac{2.8}{17}$	Levee												

-0.01 ft

Δ

1811

| | Elev | Grade | Left | | |

	Elev.	Grade	Left	C	Right
1390 Δ	7.5	21.2	$-\frac{13.4}{29.6}$ $\frac{13.4}{9}$	-13.7	$-\frac{13.1}{9}$ $-\frac{8.0}{21}$ $-\frac{2.4}{32}$ Levee
			$\frac{15.1}{31.6}$ $-\frac{14.5}{9}$	-14.6	$\frac{14.7}{9}$ $-\frac{8.1}{21.2}$ $-\frac{2.3}{30}$ Levee
+52	6.6	21.2			
+50	4.3	21.2		-16.9	
+48	6.2	21.2		-15.0	
1389	6.9	21.2	$-\frac{14.2}{30.2}$ $-\frac{14.1}{9}$ $-\frac{14.0}{9}$	-14.3	$-\frac{13.6}{9}$ $-\frac{13.5}{9}$ $-\frac{13.1}{13}$ $-\frac{8.9}{29.9}$ $-\frac{1.8}{33}$ Levee
+82	5.6	21.2		-15.6	
+80	7.6	21.2		-13.6	
+50	7.2	21.2 Δ	$-\frac{13.7}{29.6}$ $-\frac{13.7}{9}$	-14.0	$-\frac{13.0}{9}$ $-\frac{12.3}{19}$ $-\frac{10.1}{29.2}$ $-\frac{2.4}{37.0}$ Levee
1388	8.0	21.2			
			$-\frac{14.5}{30.6}$ $-\frac{13.7}{9}$	-13.2	$-\frac{12.6}{9}$ $-\frac{12.4}{15}$ $-\frac{10.8}{19}$ $-\frac{14.2}{24}$ $\frac{10.5}{24.1}$ $-\frac{2.9}{37}$ Levee
+50	8.2	21.2	$-\frac{14.1}{30.2}$ $-\frac{13.4}{9}$	-13.0	$-\frac{12.3}{9}$ $-\frac{11.5}{19}$ $-\frac{9.3}{23.0}$ $\frac{2.5}{37}$ Levee

-0.014

1813

Pages 44 To 45 Used In
Final Estimate No. 203.

1814

	Elev.	Grade	Left	C	Right
+10	8.4	21.1	$-\frac{12.2}{30.3}-\frac{13.2}{19}-\frac{13.2}{9}$	-12.4	$-\frac{10.3}{9}-\frac{11.9}{19}-\frac{10.4}{24.5}-\frac{8.5}{29}-\frac{2.5}{39}$ Level $\frac{4.8}{44.5}$
1396	8.2	21.1	$\frac{13.4}{28.1}\ \frac{13.1}{9}$	-12.9	$-\frac{12.4}{9}-\frac{11.5}{19}\ \frac{10.2}{30.4}\ \frac{8.9}{30.9}\ \frac{9.6}{39}\ \frac{2.4}{44}$ Level
+50	8.0	21.1	$-\frac{13.2}{28.8}-\frac{13.1}{9}$	-13.1	$-\frac{12.7}{9}-\frac{12.5}{19}-\frac{11.8}{26.7}-\frac{3.2}{45}$ Level

-0.014

"S" 1169+66.5 △ on Tang. See Transit Book #4, page 17

"E" 1394+09.0 △ on 1°30' curve See Level Book #6, page 13

See Original Cross Section Book № 7, page 64, S" Line.

See Final Cross Section Book № 6, page 3 to 4.

1395 △	7.8	21.1	$-\frac{14.3}{34.5}\ \frac{14.1}{9}$	-13.9	$-\frac{13.2}{9}-\frac{13.3}{19}-\frac{12.7}{26.1}-\frac{3.5}{49}$ Level
+50	8.1	21.1	$-\frac{12.8}{38.2}-\frac{12.8}{9}$	-13.0	$-\frac{12.1}{9}-\frac{11.5}{26.3}-\frac{2.7}{46}$ Level
1394	8.2	21.2	$-\frac{13.2}{28.8}-\frac{13.2}{9}$	-13.0	$-\frac{12.3}{9}-\frac{11.2}{25.8}-\frac{2.6}{43}$ Level
+50	7.8	21.2	$\frac{13.8}{29.7}-\frac{13.8}{9}$	-13.4	$-\frac{13.1}{9}-\frac{11.9}{19}-\frac{10.5}{25.2}-\frac{1.4}{42}$ Level

1815

	Elev	Grade	Left	℄	Right
+50	6.3	21.1		-14.8	
+45	7.3	21.1		-13.8	
+40	9.5	21.1	0.014	-11.6	
+05	4.1	21.1		-17.0	
B.M.	13.889	21.1	On Oak tree 66 ft. R. 1397.		
1397	8.5	21.1		-17.6	
+95	3.9	21.1		-17.2	
+85	9.5	21.1		-11.6	
+68	16.0	21.1		-5.1	
+65 Δ	16.1	21.1	Δ	$-\frac{14}{20.1}$ $-\frac{6.8}{9}$	-5.0 $-\frac{4.0}{9}$ $-\frac{4.0}{15.0}$
+57	16.1	21.1		$-\frac{5.2}{16.8}$ $-\frac{5.0}{9}$	-5.0 $-\frac{4.0}{9}$ $-\frac{4.0}{15.0}$
+50	11.2	21.1		$-\frac{11.0}{25.5}$ $-\frac{11.0}{19}$ $-\frac{10.1}{9}$	-9.9 $-\frac{6.5}{9}$ $-\frac{4.0}{12.0}$ $-\frac{4.0}{15.0}$
+40	6.8	21.1		$-\frac{16.2}{33.3}$ $-\frac{16.2}{29}$ $-\frac{15.9}{19}$ $-\frac{15.4}{9}$	-14.3 $-\frac{10.8}{9}$ $-\frac{6.8}{19.2}$

1816

	Elev	Grade	Left	C	Right
1400	7.8	21.1		-13.3	
+75	13.5	21.1	-0.014	-7.6	
+50	14.1	21.1		-7.1	
+08	12.0	21.1		-9.1	
1399 Δ	10.4	21.1 Δ		-10.7	
+90	8.0	21.1		-13.0	
+50	7.5	21.1		-13.3	
1398	7.7	21.1		-13.4	

18171

1382+17 -17- 1371+18 -7- 1373+25 -15- 1378+60 -33- 1377+77 -18- 1379+73 -12- 1381+91 -14- 1383+91 -22- 1385+21 -8- 1380+67 -8- 1377+54 -8- 1374+71 -17- 1376+20 -14- 1378+01 -4- 1380+22 -4-

1818

67

483 + 79 =	Bent No 13	End of Bank
+ 64 =	Bent No 12	
+ 49 =	Bent No 11	
+ 34 =	Bent No 10	
+ 19 =	Bent No 9	
483 + 04 =	Bent No 8	
+ 89 =	Bent No 7	
+ 74 =	Bent No 6	
+ 59 =	Bent No 5	
+ 44 =	Bent No 4	
+ 29 =	Bent No 3	
+ 14 =	Bent No 2	
482 + 00	Bent No 1	(End of Bank)

13 Bent Trestle on Pile Foundation — 12 - Spans

473 + 36 =	Bent No 7	(End of Bank)
473 + 22 =	Bent No 6	
473 + 07 =	Bent No 5	
472 + 92 =	Bent No 4	
+ 77 =	Bent No 3	
+ 62 =	Bent No 2	
472 + 47 =	Bent No 1	(End of Bank)

7 Bent Trestle on Pile Foundation 6 - Spans

1819

1820

1
13°8'
P.I.
1821